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Introduction

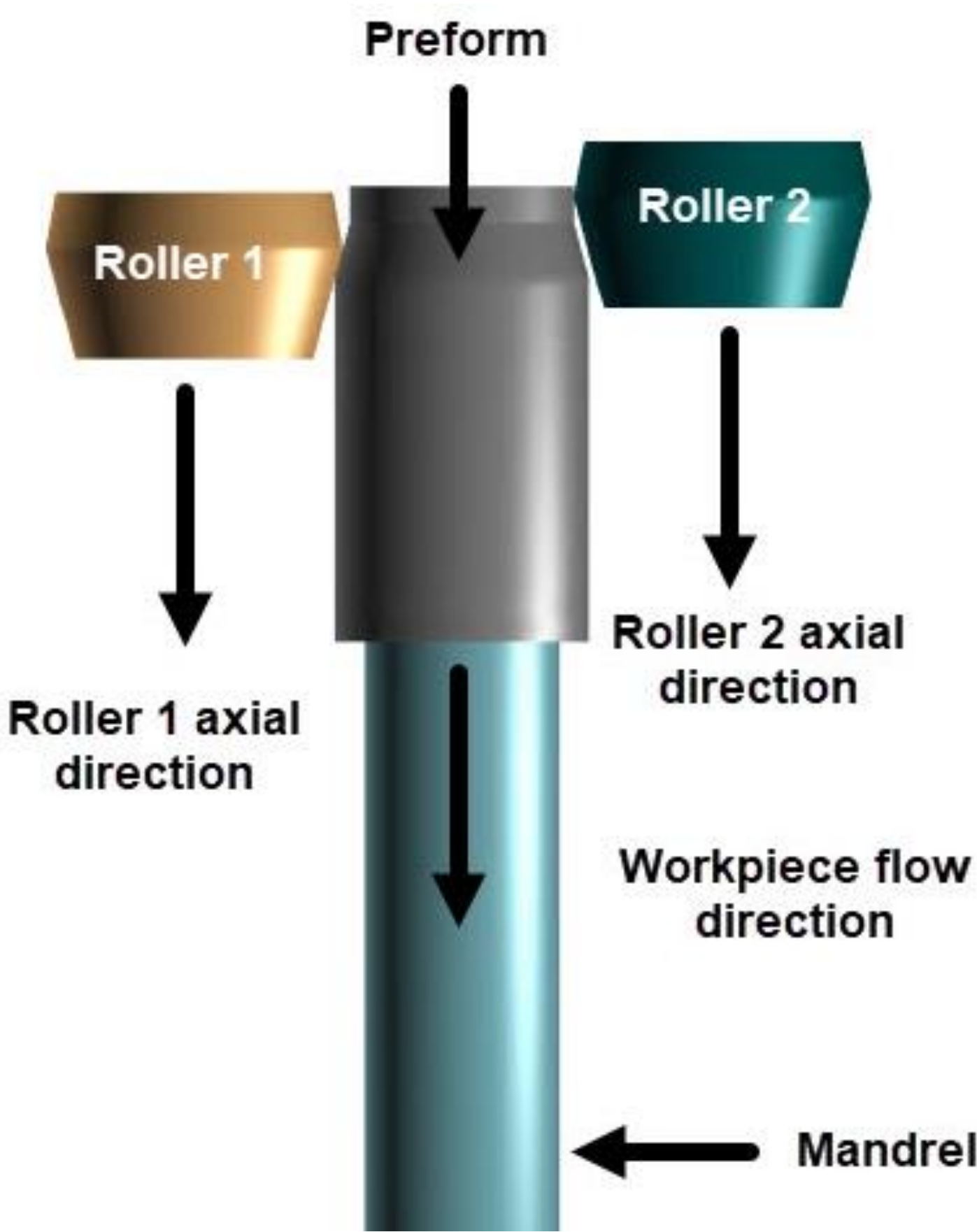


Figure 1 Designation of two roller staggered vertical forward tube flow forming process

Finite Element Model

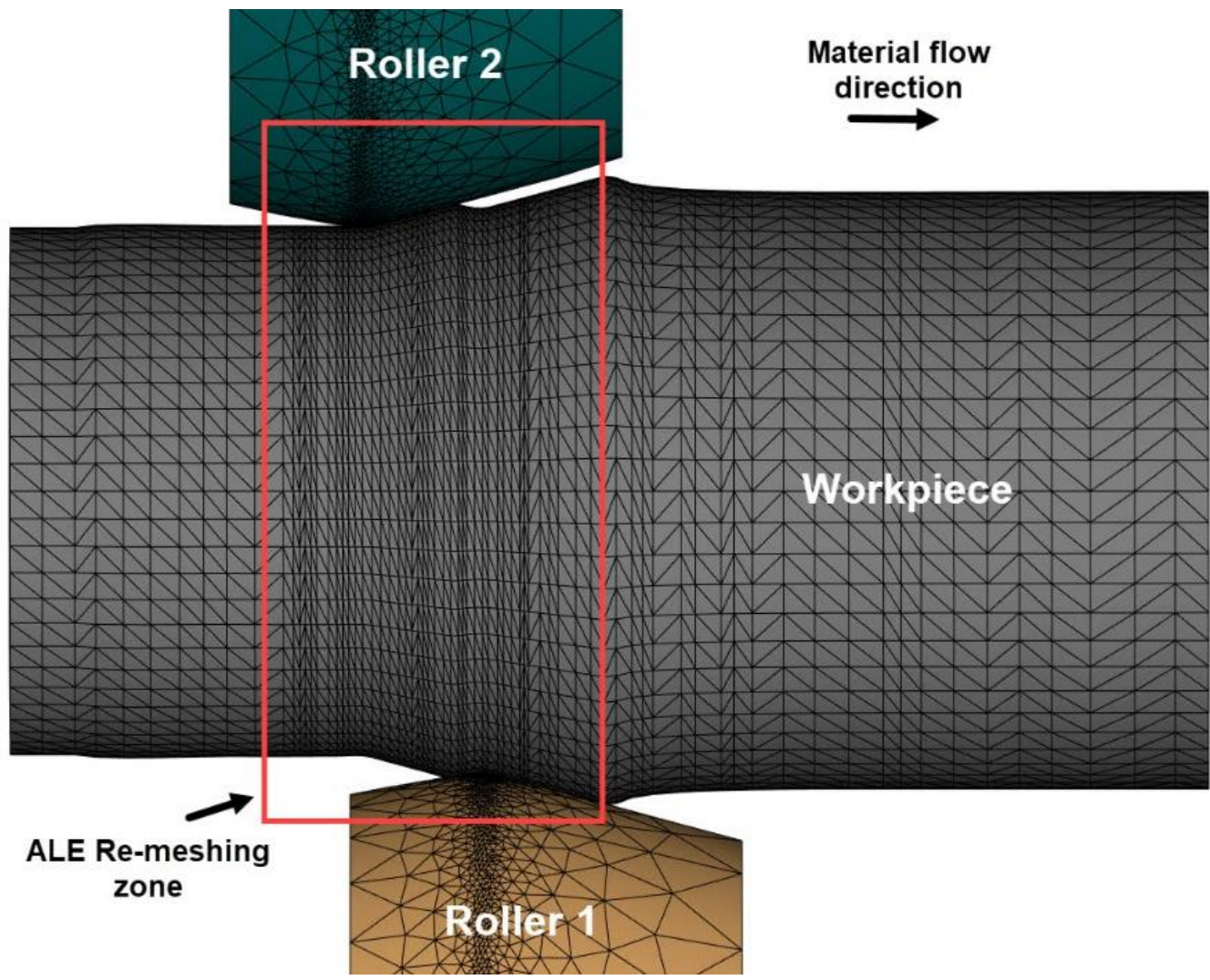


Figure 2 Workpiece re-meshing zone during the forward flow forming process

Re-meshing Model

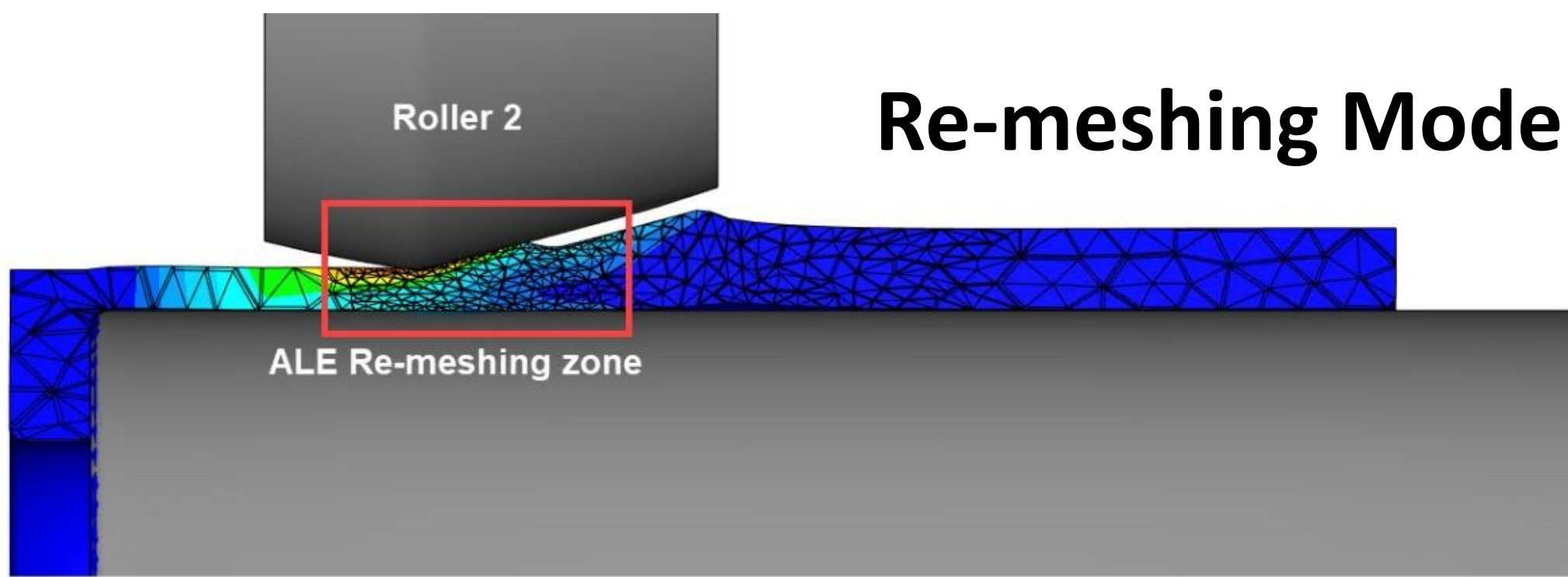


Figure 3 Cross-section of structured ALE re-meshing under the roller

Equations

Law Limited Tresca friciton model

$$\tau = \mu \sigma_n \begin{cases} \text{If } \mu \sigma_n < \bar{m} \frac{\sigma_0}{\sqrt{3}} & \text{then } \tau = \mu \sigma_n \\ \text{If } \mu \sigma_n \geq \bar{m} \frac{\sigma_0}{\sqrt{3}} & \text{then } \tau = \bar{m} \frac{\sigma_0}{\sqrt{3}} \end{cases}$$

$$C_{CR} = \int_0^{\bar{\epsilon}_f} \left(\frac{\sigma_{max}}{\bar{\sigma}} \right) d\bar{\epsilon}$$

Von Mises Stress

$$\sigma_{eq} = \frac{1}{\sqrt{2}} [(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_1 - \sigma_3)^2]^{\frac{1}{2}}$$

$$\tau = \mu (\Delta \cdot v \sigma_n) \Delta v$$

$$m = m_0 + m_1 T$$

$$\varphi_c = h(T - T_0)$$

$$\dot{W} = \eta c_{ij} \dot{\epsilon}_{ij} = \eta K \sqrt{3} \dot{\epsilon}^{m+1}$$

FEA Method

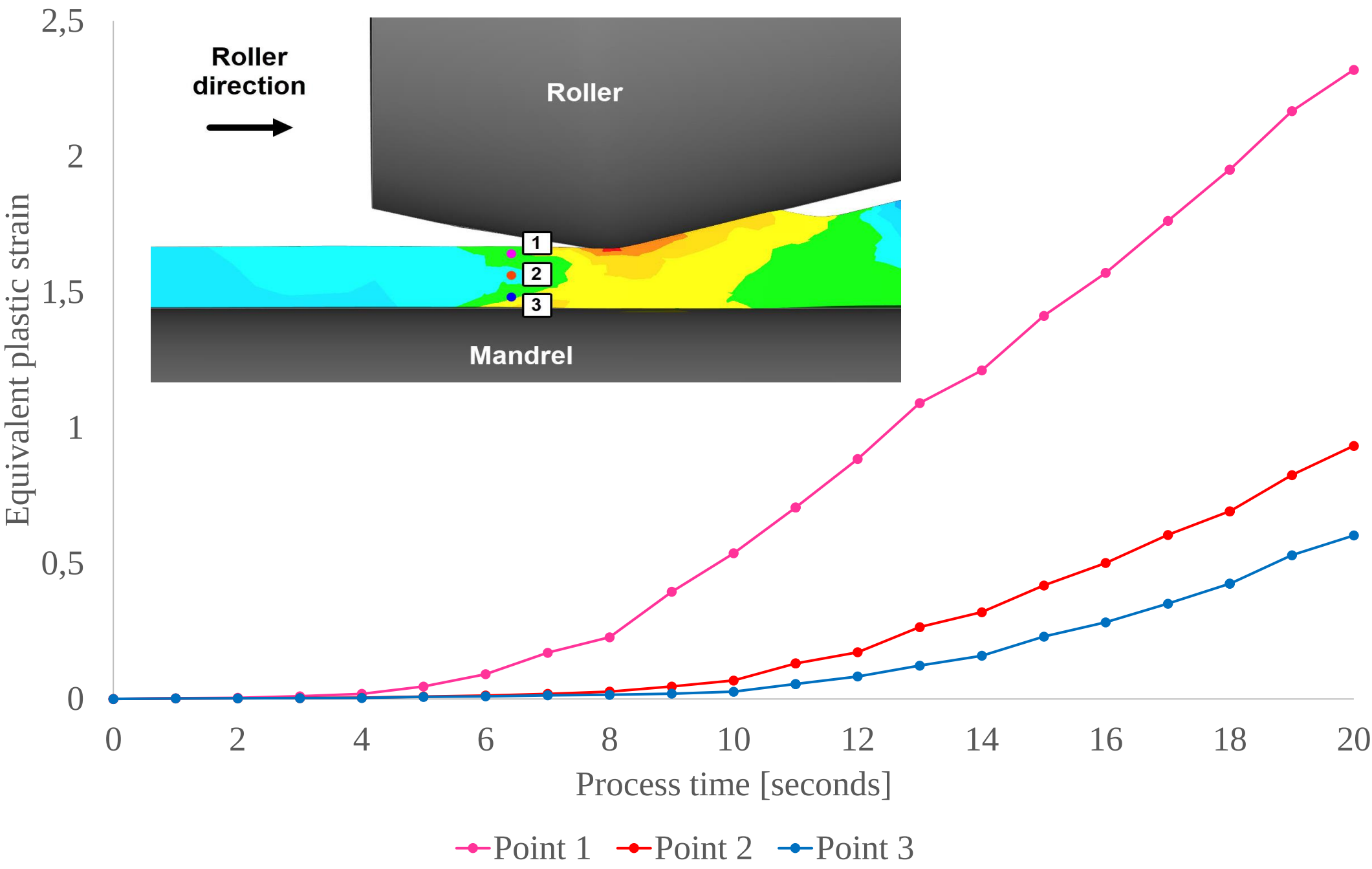


Figure 4 Strain distribution through the wall thickness from outside (Point 1) to inside surface (Point 3)

Experimental Results

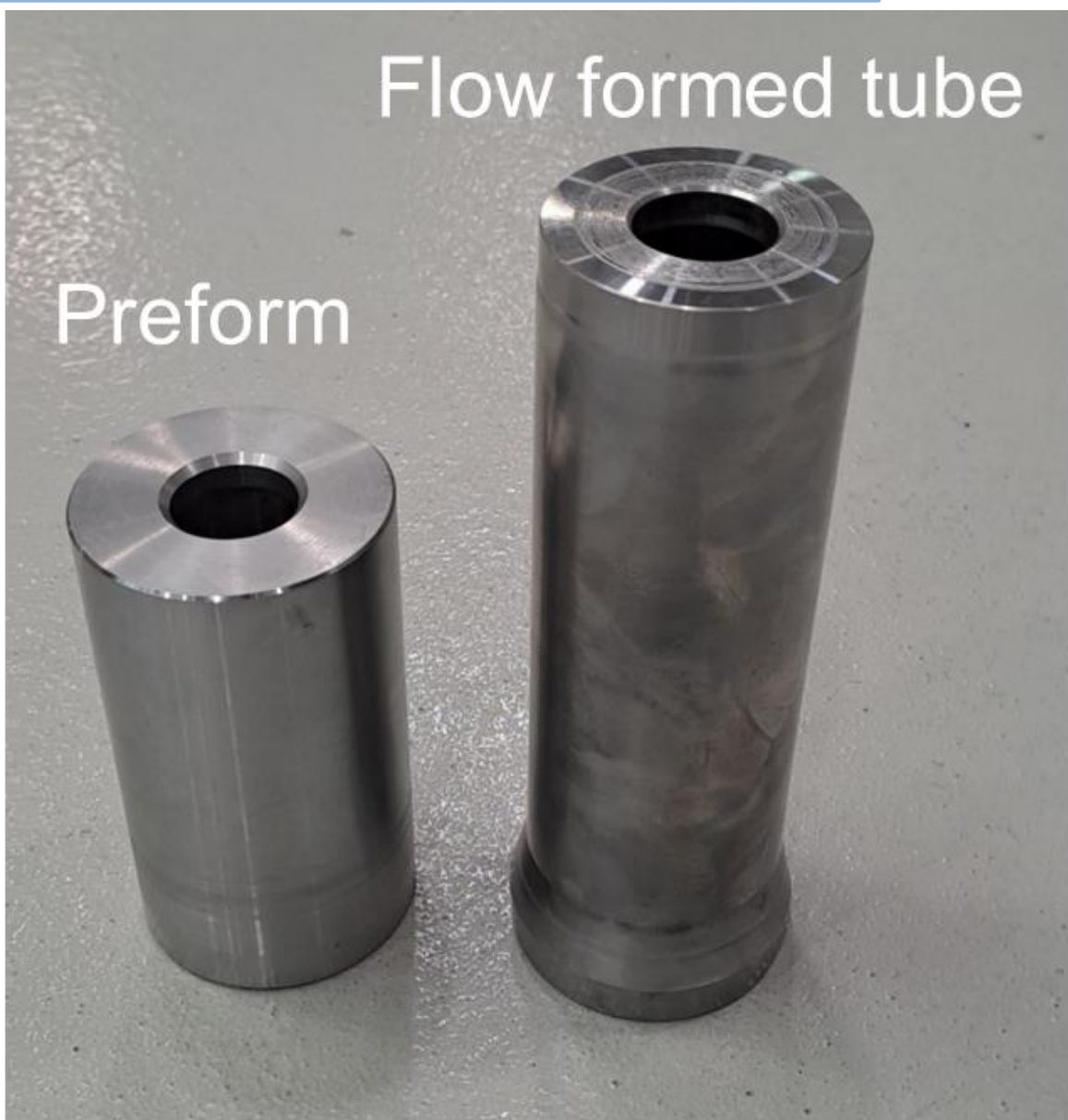


Figure 5 Preform and flow formed tube pictures after the flow forming process

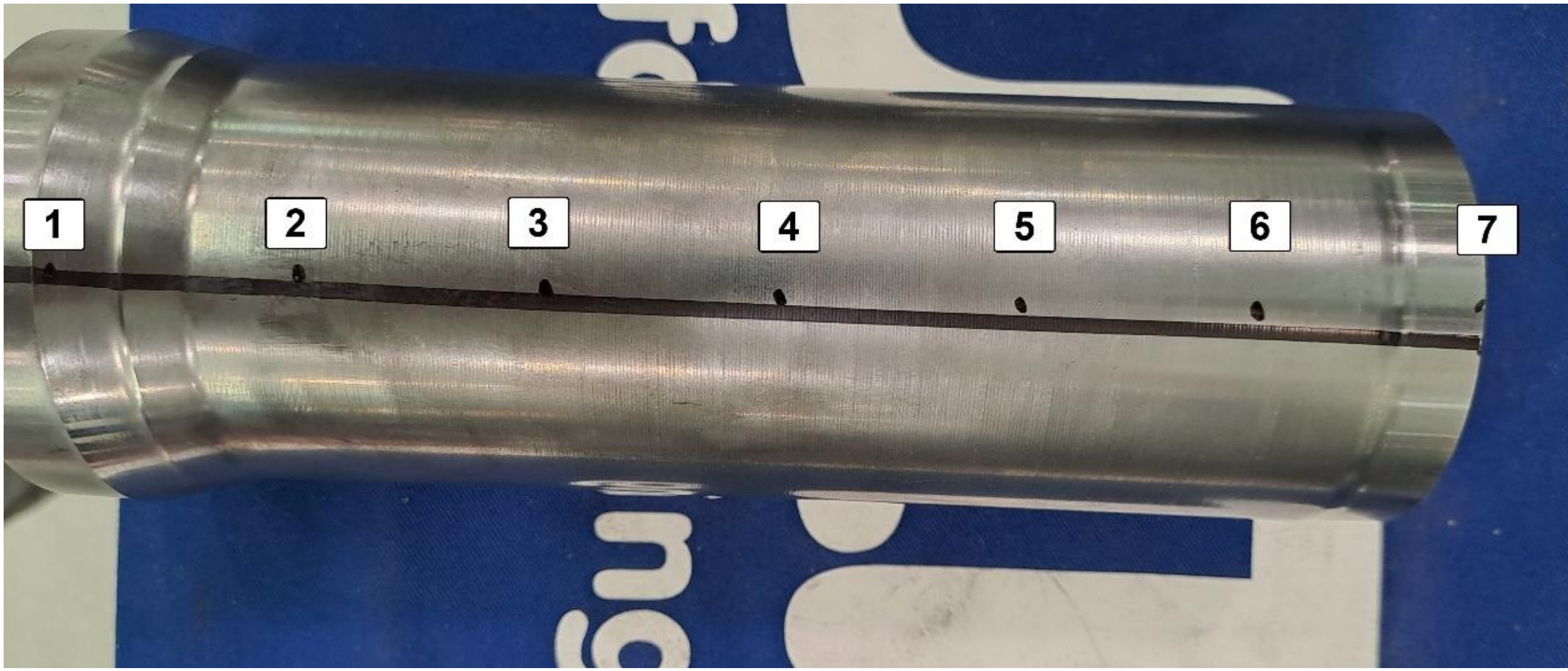


Figure 6 Twist measurement points of flow formed tube with 30 mm intervals

Twist measurement

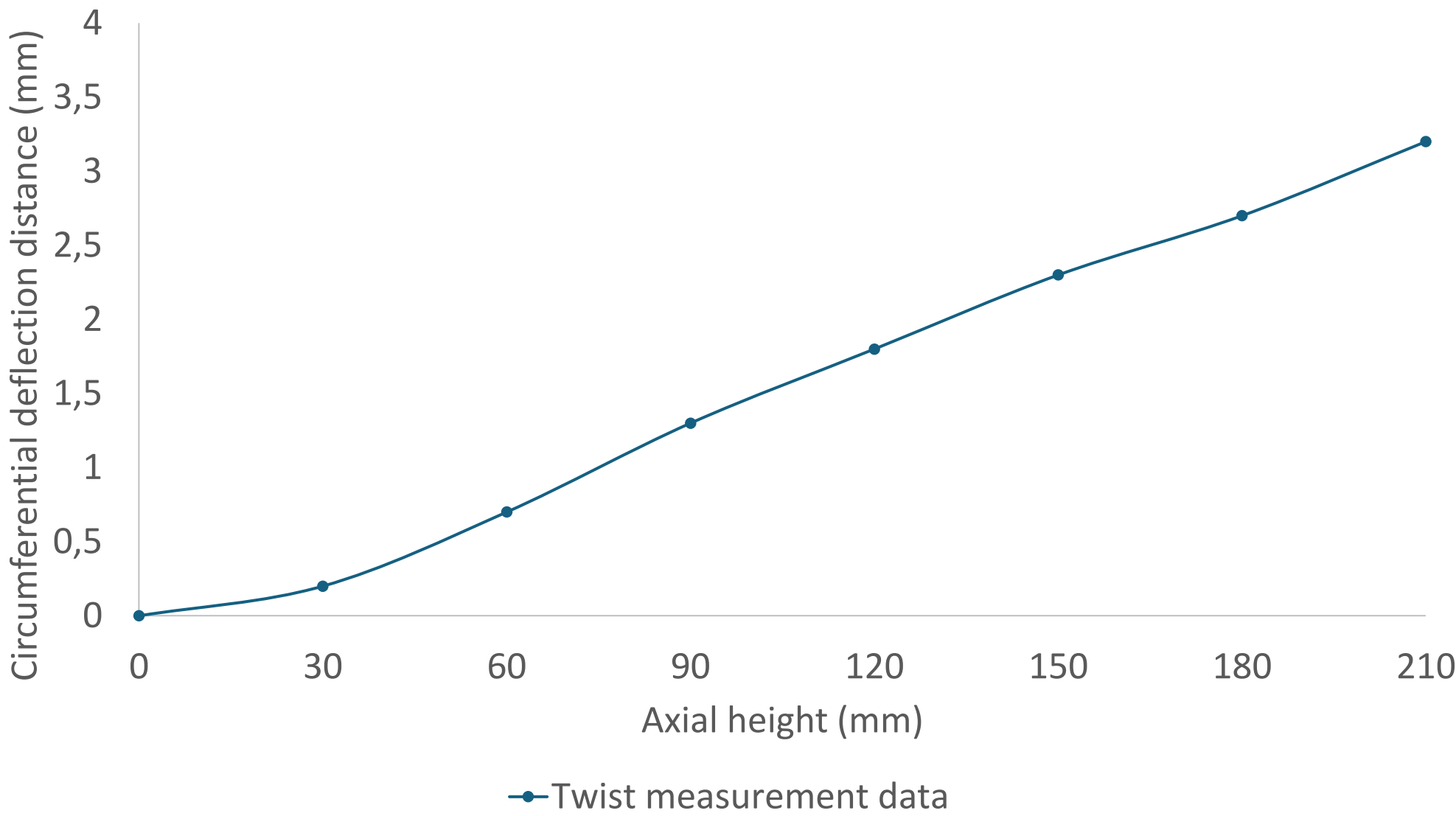


Figure 7 Twist results of each point after the flow forming process

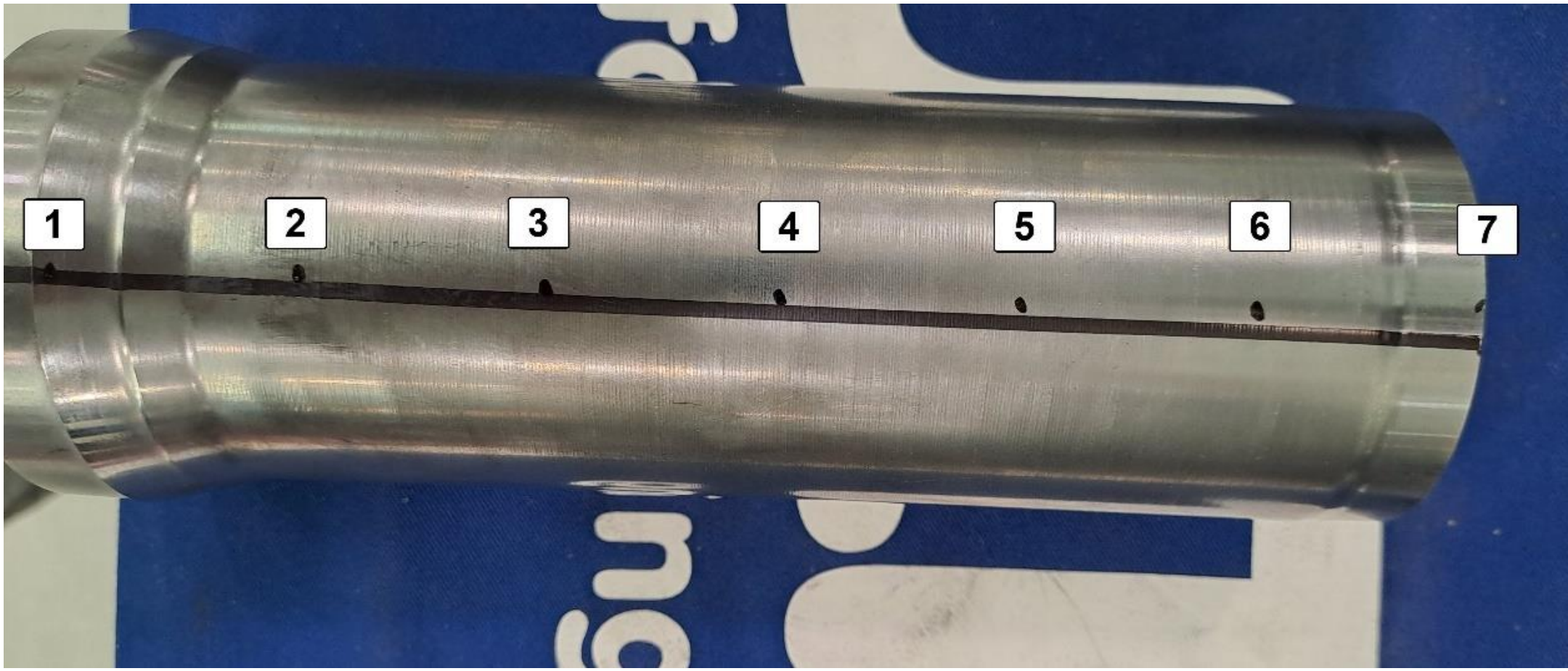


Figure 8 Comparison of average hardness between the simulation and experiment

Conclusions

- The FEA results have demonstrated good agreement with the experiments regarding stress, strain, and damage results. It was verified that the outside surface of the workpiece exhibited a greater strain value, gradually diminishing towards the inner diameter of the workpiece
- The present research indicates that the ALE formulation is very proficient in simulating the flow forming process, yielding highly precise predictions of the workpiece hardness.
- The twist indicates a consistent effect of the flow-forming process along the tube's length, with each segment gradually undergoing increased deformation.

References

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2. F. Li, C. Zhu, S. Zhao, Research on a new counter-roller active spinning process for forming Al alloy thin-walled cylinders, J. Mater. Process. Technol. 326 (2024) 118309. <https://doi.org/10.1016/j.jmatprotec.2024.118309>.

3. P.F. Gao, M. Li, M. Zhan, L. Xing, F. Ma, M.W. Fu, Circumferential twist in flow forming of tubular parts: Characterization, understanding and control, J. Manuf. Process. 65 (2021) 144–152. <https://doi.org/10.1016/j.jmapro.2021.03.020>

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