

Predicting initial in-situ stresses in dam sites using an advanced meta model



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Introduction

The initial in-situ stresses in dam sites are an important factor that affects the safety of the dam, and predicting them accurately and reliably helps to understand the behaviour of the dam and its foundation. In this study, an advanced meta-modelling technique, the Polynomial Chaos Kriging (PCK) model, is used to predict the initial in-situ stresses in dam sites. The constructed PCK model not only provides higher prediction accuracy compared to traditional multiple linear regression models, but also performs parameter sensitivity analysis at near-zero cost.

Methods

➤ PCK

$$Y \approx \mathcal{M}^{PCK}(X) = \sum_{w \in \Omega} \zeta_w \delta_w(X) + \sigma^2 D(x)$$

PCE

Kriging

The weighted sum of orthogonal polynomials

The variance of a zero-mean stationary Gaussian process

- (1) determining the truncated polynomial set

(2) calibrating the unknown Kriging hyper-parameters

In PCK, a **regression-type PCE model** is employed to capture the global behavior of the computational model, while an **interpolation-based Kriging model** is utilized to capture local variations in the computational model.

Graphics / Images

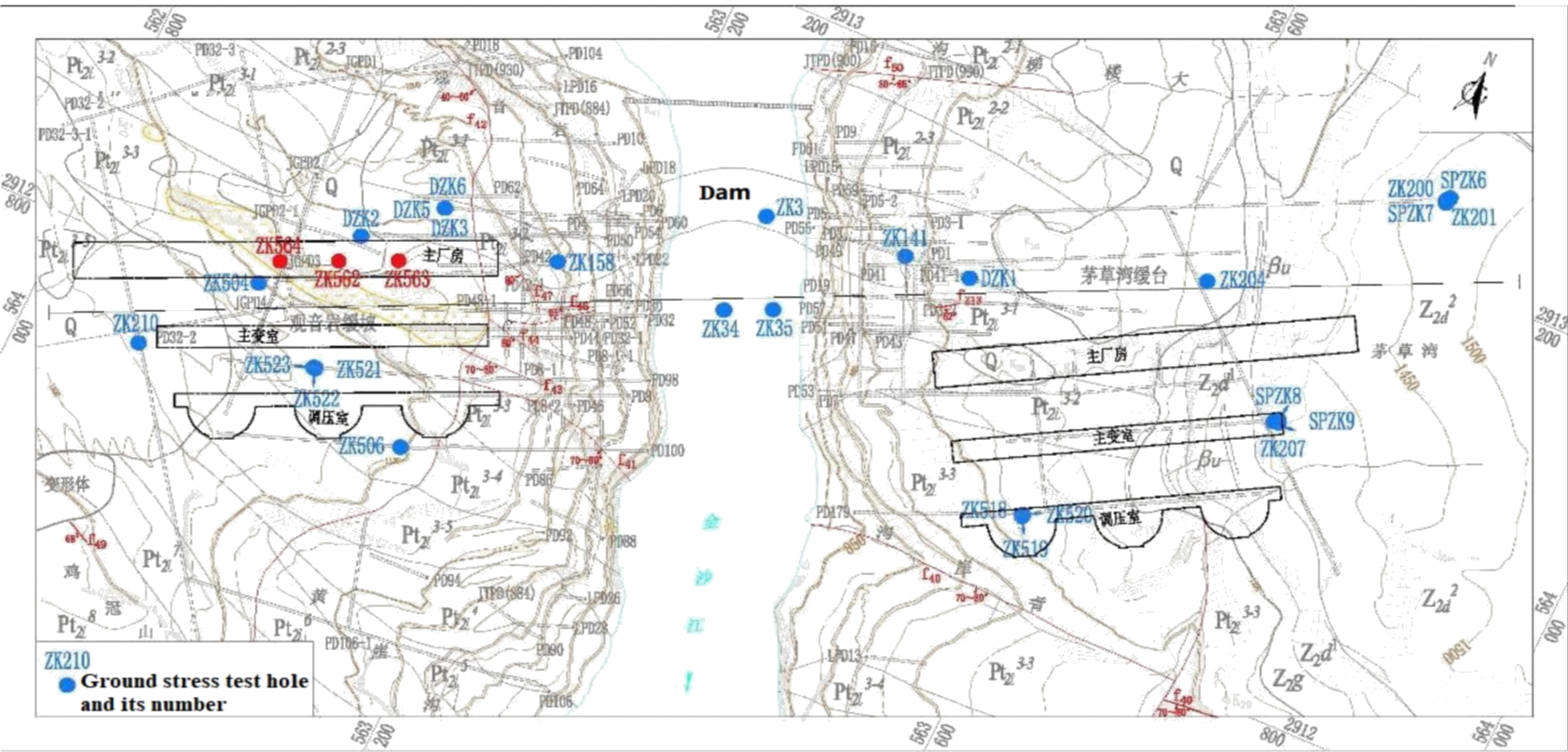


Figure 1. Graph of borehole locations for in-situ stress measurements in the dam site area

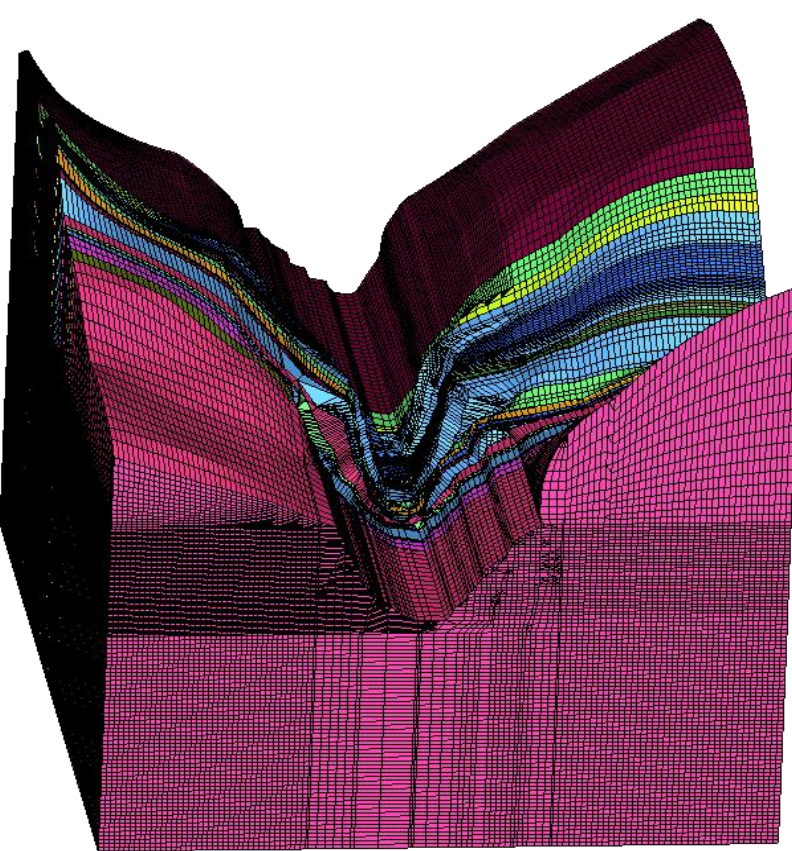


Figure 2. Finite element model of the refined dam site area

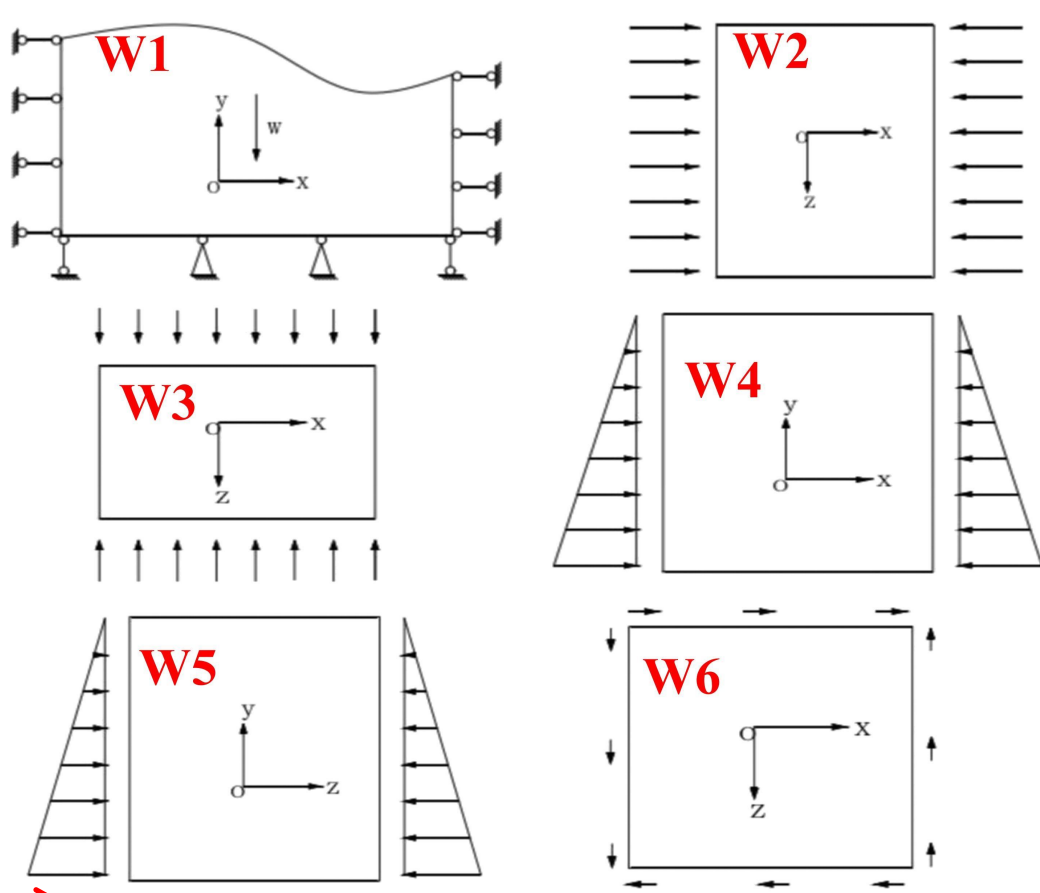


Figure 3. Boundary condition scenarios for simulating the in-situ stress field

- W1: Self-weight
- W2: East-West uniform extrusion structure
- W3: North-South uniform compression structure
- W4: East-West triangular load extrusion structure
- W5: North-South triangular load extrusion structure
- W6: Uniform shear tectonic stress in the horizontal plane

		Input						Output	
		Measurement point number	W1	W2	W3	W4	W5	W6	measured stress component
Training dataset	1	X1 (sx)	-1.6128	-0.2486	-1.0972	-0.5237	0.4475	1.0973	3.1783
		X2 (sy)	-0.8494	-0.0898	-6.5144	0.1921	0.1542	6.5144	5.4864
		X3 (sxy)	0.1734	0.0349	0.9284	0.8299	0.0606	-0.9284	3.5209
		X4 (sz)	-4.9936	-0.1772	0.2820	0.3074	0.4407	-0.2820	2.9267
		X5 (sxz)	1.8262	0.2278	0.0154	0.2967	-0.3839	-0.0154	3.2393
		X6 (syz)	-0.0887	-0.0119	0.9768	-0.9924	-0.0555	-0.9768	1.8683
	2	X1	-1.4795	-0.2319	-0.9458	-0.4779	0.3962	0.9458	3.1601
		X2	-0.7675	-0.0745	-5.9629	0.7353	0.1201	5.9630	5.7890
		X3	0.1087	0.0315	0.6732	0.2242	0.0434	-0.6732	3.0480
		X4	-4.9284	-0.1856	0.3095	0.3233	0.4492	-0.3095	2.9542
		X5	1.7887	0.2241	-0.0008	0.2741	-0.1827	0.0008	3.2202
		X6	-0.0768	-0.0140	0.8628	-0.9897	-0.0588	-0.8628	1.9139
	3	X1	-0.1453	-0.0226	0.0191	0.0824	0.0382	-0.0191	3.1893
		X2	-0.4883	-0.0018	-4.7438	0.4400	0.0643	4.7438	5.0292
		X3	-0.2074	-0.0119	-0.0732	0.3023	0.0746	0.0732	3.3978
		X4	-4.1563	-0.0531	0.9319	0.1897	0.4381	-0.9319	2.5112
		X5	0.9349	0.0798	-0.1678	-0.1100	-0.1820	0.1678	3.1295
		X6	0.2031	0.0254	0.3070	-0.8049	-0.0634	-0.3070	2.2426
	4	X1	-1.1459	-0.1453	-0.6176	0.1540	-0.1131	0.6176	3.5326
		X2	-1.2806	-0.0477	-7.7252	0.0322	0.0085	7.7252	5.6172
		X3	-0.0031	-0.0192	0.2725	0.6505	-0.0989	-0.2725	3.6404
		X4	-4.2457	-0.0544	-0.3170	0.0940	0.0113	0.3170	2.8259
		X5	1.2999	0.0896	0.3283	-0.0666	-0.2731	-0.3283	2.9545
		X6	-4.2457	-0.0544	-0.3170	0.0940	0.0113	0.3170	2.8259
5	X1	-0.8534	-0.0167	-0.9250	-0.5679	-0.4368	0.9250	2.7980	
	X2	-0.8204	-0.0036	-3.8085	0.4712	-0.0788	3.8085	4.7041	
	X3	0.5838	0.0085	2.5602	-0.4763	-0.0342	-2.5601	1.8684	
	X4	-4.0544	-0.0195	0.2757	-0.2390	-0.1475	-0.2757	2.2886	
	X5	1.4615	0.0158	-0.8997	0.5871	0.1715	0.8997	4.1109	
	X6	-0.9909	-0.0072	0.9651	-0.6424	-0.1493	-0.9651	2.0683	
6	X1	-2.8005	-0.2602	-1.6605	0.6042	-1.3002	1.6605	4.2528	
	X2	-1.9557	-0.1072	-0.0918	0.0673	0.1734	0.0918	6.1141	
	X3	-0.4557	-0.0405	-1.6619	0.9514	-0.0981	1.6619	4.5379	
	X4	-7.2967	-0.1769	-0.1703	-0.1703	-0.5471	0.1703	2.3256	
	X5	-3.3771	-0.2447	-0.0698	0.3522	-0.7714	0.0698	3.3944	
	X6	-0.6131	0.0048	0.6831	1.1969	0.1213	-0.6831	3.8907	
7	X1	-0.7844	-0.0168	-0.2761	0.1721	-0.2266	0.2761	3.2748	
	X2	-1.1711	-0.0143	-7.1707	0.3045	-0.0020	7.1707	5.6437	
	X3	-0.3841	-0.0037	0.3521	0.1956	0.0378	-0.3521	3.1209	
	X4	-1.9440	-0.0133	-0.8197	0.0986	-0.1168	0.8197	3.2320	
	X5	-1.0792	-0.0089	-0.2714	0.1452	-0.1302	0.2714	3.1982	
	X6	-0.9097	-0.0053	-0.9329	0.4827	-0.0139	0.9329	3.7474	
8	X1	-2.2451	-0.2923	-0.8931	0.0350	-0.3269	0.8931	3.6096	
	X2	-0.2025	-0.0930	0.2734	0.8299	-0.0761	10.3971	5.0091	
	X3	-2.4786	-0.0030	-10.3971	0.0719	0.0571	-0.2734	5.1458	
	X4	-8.8984	-0.0094	0.6391	0.1516	-0.0717	-0.6391	1.9739	
	X5	-2.9343	-0.1977	-0.5961	0.0724	-0.3572	0.5961	3.2981	
	X6	-1.0427	0.0154	-0.4415	0.7179	0.0446	0.4415	3.7501	

Figure 4. Initial dataset for constructing the PCK model

- Input: The six-direction stress components of each measured point under six different boundary condition.

Output: The measured in-situ stress components of each measured point.

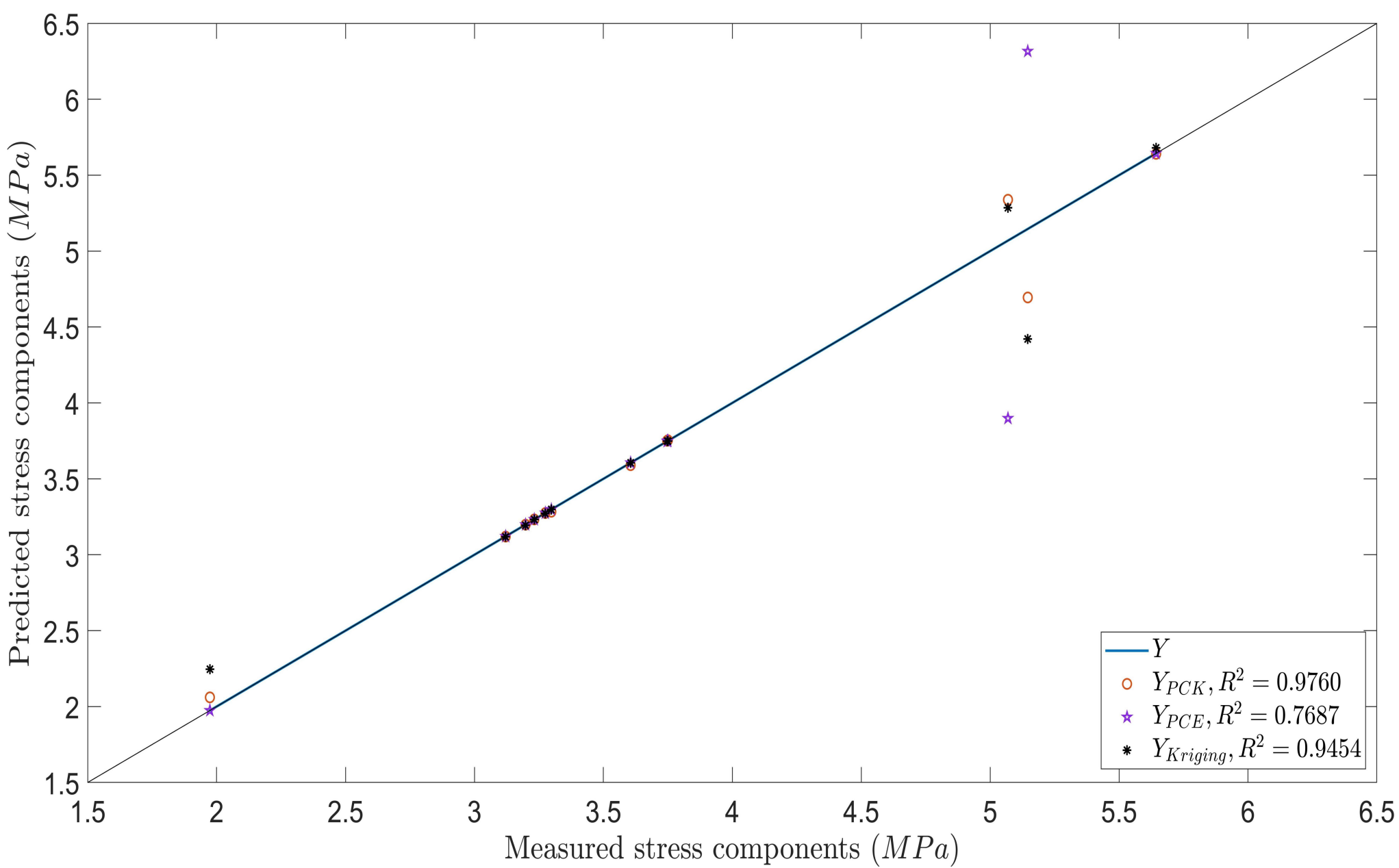


Figure 5. The predictive accuracy of in-situ stress based on the PCK model

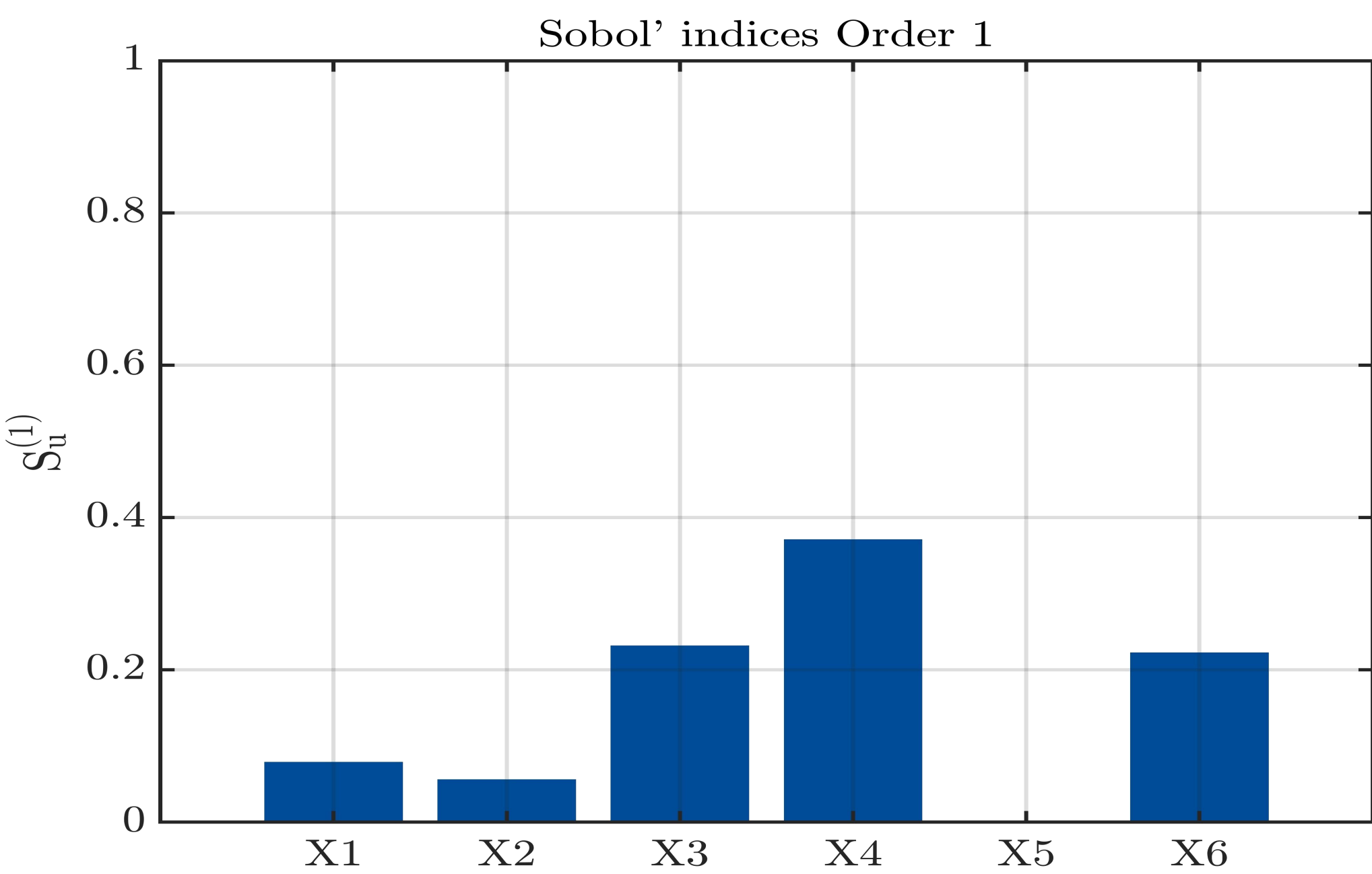


Figure 6. Sensitivity analysis of input parameters based on PCK model

Conclusions

- From Figure 5, compared to the PCE and Kriging models, the PCK model demonstrates higher accuracy and stronger capability for modeling with small samples, indicating its good practicality in engineering applications.

➤ From Figure 6, according to the sensitivity analysis results, the stress component corresponding to the SZ-direction has the most significant impact on the output response. This is consistent with the fact that the initial in-situ stress is primarily influenced by self-weight.